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ARTICLE

Controllable Synthesis of Polycrystalline Nanostructure TiO₂ by Gaseous-Liquid Detonation Method

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Abstract: The polycrystalline nano-TiO₂ was synthesized by the gaseous-liquid detonation (GLD) method using H₂, O₂, and TiCl₄ as the mixture precursors. The effects of different molar ratios of precursors and initial reaction pressures on the nano-TiO₂ crystalline structures were studied. The nanocrystal structures, components, particle size, and morphology were characterized by the X-ray diffraction (XRD) and transmission electron microscopy (TEM). The results demonstrate that the nano-TiO₂ consists of pure anatase-TiO₂, pure rutile-TiO₂, and the mixtures of spherical or quasi-spherical morphologies with particle size of 20~150 nm. Furthermore, the formation mechanism of nano-TiO₂ by GLD method was analyzed. The relevant GLD parameters were calculated based on the C-J theory and the related chemical reaction data, which effectively verifies the influence of different molar ratios of precursors and initial pressures on the controllable synthesis of polycrystalline nano-TiO₂.

Key words: nano-TiO₂; gaseous-liquid detonation; polycrystalline nanostructure; detonation parameters; C-J theory

Nano-TiO₂ is one of the most extensively used nanomaterials due to its stable chemical structure, biocompatibility, and physical, optical, and electrical properties, and it is normally used in catalysis^[1-3], Li-ion batteries^[4-6], gas sensors^[7,8], and antibacterial active materials^[9,10]. Generally, the TiO₂ crystals have three polymorphic phases: anatase, rutile, and brookite. The anatase and rutile are two important structures of TiO₂ used in commercial products^[11]. The pure nano-TiO₂ is often prepared by hydrothermal synthesis, flame method, and chemical vapor deposition (CVD) method. Hydrothermal method can synthesize different TiO₂ nanocrystals under the hydrothermal environment. Lin et al^[12] fabricated a series of mixed-phases of TiO₂ by hydrothermal synthesis using TiCl₃ as the precursor and ammonia water for regulating the ratio of different crystal phases. Flame method can adjust the component, size, and morphology of nanomaterials. Wu et al^[13] explored the transformation of nano-TiO₂ crystal phase and fabricated pure

anatase-TiO₂ by changing the flame gas flow rates of the fuel, oxygen, and argon carrier. CVD method is widely used to prepare nano-TiO₂, because it can easily control the crystal type and morphology by adjusting the gas ratio and dosage of catalyst. Chen et al^[14] reported that rutile-TiO₂ nanowires are grown on the Ti foil through controlling the growth temperature and the thickness of the catalyst layer which is important for activating the surface of Ti foil and facilitating the TiO₂ growth in CVD system.

However, these conventional techniques require long time for production and advanced equipment. Compared with these techniques, the gaseous-liquid detonation (GLD) method has its unique advantages of simple operation and provides the high temperature and high pressure conditions for rapid reaction and growth of nanomaterials^[15-17]. Luo et al^[18,19] used H₂, O₂, C₂H₆O, and TiCl₄ as the precursors to prepare TiO₂ and discussed the growth of spherical TiO₂ during rapid detonation reaction process. Wu et al^[20,21] synthesized SnO₂-TiO₂

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nanocomposites and nano-Fe₂O₃-TiO₂ composites by detonation method, and investigated the influence of Sn⁴⁺ and Fe³⁺ on the crystalline structure of nano-TiO₂. Nevertheless, the synthesis mechanism of crystalline structure of nano-TiO₂ is still unclear, which greatly restricts its industrial production.

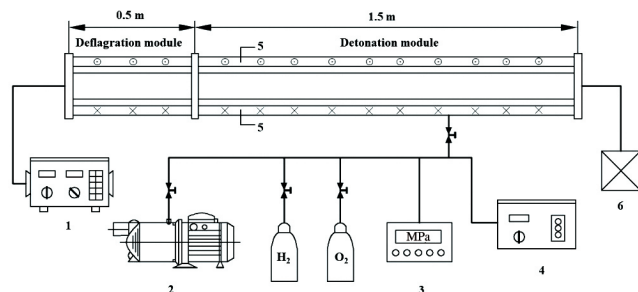
In this research, different nano-TiO₂ crystals were prepared by GLD method through adjusting the precursor (H₂, O₂, TiCl₄, and C₂H₆O) content and initial pressure. The X-ray diffraction (XRD) and transmission electron microscopy (TEM) were used to characterize the crystalline structure, components, particle size, and morphology of nano-TiO₂. Furthermore, by combining C-J theory with chemical reaction data, different crystalline structures of nano-TiO₂ were analyzed.

1 Experiment

The polycrystalline nano-TiO₂ was prepared in the GLD system, as shown in Fig. 1. The GLD tube consisted of two modules with different lengths, namely the deflagration module of 0.5 m in length and the detonation tube module of 1.5 m in length. The shock tube was made of titanium alloy and the inner diameter was 0.1 m.

In a typical preparation procedure, the GLD tube was heated to 380~550 K after vacuuming (barometer reading-0.09 MPa). A certain amount of TiCl₄ solution was injected by the atomizer into the tube. Then the mixed gas with a certain proportion of H₂ and O₂ was pumped into the GLD synthesis system until reaching the atmosphere pressure. The gaseous-liquid mixtures were placed statically for 5~10 min and then ignited using the electric igniter of 20~40 J. Finally, after the tube was cooled down to room temperature, the white products were collected from the inner wall of GLD tube and washed with absolute ethanol.

The nano-TiO₂ phases and crystalline structure of the detonation products were characterized by D/MAX 2400 XRD (Cu Kα, λ=0.154 06 nm). The tube voltage was 40 kV, the tube current was 30 A, and the scanning range was 20°~80°. The morphologies of nano-TiO₂ structure were observed using TEM (Tecnai F30, FEI) with point resolution of 0.2 nm and line resolution of 0.1 nm.

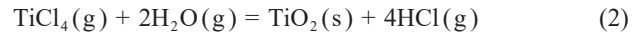
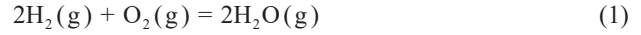


1-high energy igniter; 2-vacuum pump; 3-barometer; 4-liquid atomizing system; 5-temperature control system; 6-exhaust gas treatment equipment

Fig.1 Schematic diagram of GLD system

2 Calculation of GLD Parameters

The gaseous-liquid mixture precursors consisted of gas mixture and TiCl₄ was ignited by the high energy spark of 20~40 J to prepare nano-TiO₂. During the GLD process, the detonation heat, high temperature, and high pressure were generated, resulting in the fact that the mixture precursors decompose into nano-TiO₂. The related chemical reactions are as follows:



When the chemical equilibrium was attained, a steady-state detonation was achieved and its propagation rate was governed only by the thermodynamics and hydrodynamics. Assuming that a standing detonation wave is similar to the calculated shock waves, the laws of conservation of mass, momentum, and energy applied across the shock front may lead to the conservation equations^[18], as follows:

$$\rho_0(D_0 - u_0) = \rho_{\text{CJ}}(D_{\text{CJ}} - u_{\text{CJ}}) \quad (3)$$

$$P_0 + \rho_0(D_0 - u_0)^2 = P_{\text{CJ}} + \rho_{\text{CJ}}(D_{\text{CJ}} - u_{\text{CJ}})^2 \quad (4)$$

$$e_0 + \frac{P_0}{\rho_0} + \frac{(D_0 - u_0)^2}{2} = e_{\text{CJ}} + \frac{P_{\text{CJ}}}{\rho_{\text{CJ}}} + \frac{(D_{\text{CJ}} - u_{\text{CJ}})^2}{2} + Q \quad (5)$$

$$\frac{P_{\text{CJ}} - P_0}{V_0 - V_{\text{CJ}}} = \gamma \frac{P_{\text{CJ}}}{V_{\text{CJ}}} \quad (6)$$

where ρ is the gas density, D is the detonation velocity, u is the particle velocity, P is the detonation pressure, e is the specific internal energy, Q is the released specific heat from explosions, γ is the isentropic adiabatic index exponent, V is the ideal gas volume, and the subscript 0 and CJ represent the physical quantities before and after rapid reaction, respectively. Internal energy e_i can be expressed by Eq.(7), as follows:

$$e_i = \frac{P_i V_i}{\gamma_i - 1} \quad i = 0 \text{ or CJ} \quad (7)$$

Assuming that $\gamma_0 = \gamma_{\text{CJ}} = \gamma$, $P_0 \ll P_{\text{CJ}}$, the results can be calculated according to Eq.(8~11), as follows:

$$D = \sqrt{2(\gamma^2 - 1)Q} \quad (8)$$

$$P_{\text{CJ}} = \frac{\rho_0 D^2}{\gamma + 1} \quad (9)$$

$$\rho_{\text{CJ}} = \frac{\gamma + 1}{\gamma} \rho_0 \quad (10)$$

$$u_{\text{CJ}} = \frac{D}{\gamma + 1} \quad (11)$$

The calculation of gaseous detonation heat is based on Hess's law of thermochemistry. According to the first law of thermodynamics, the relationship between thermal effect at constant volume Q_v and constant thermal effect Q_p can be expressed by Eq.(12), as follows:

$$Q_v = Q_p + P(V_j - V_i) \quad (12)$$

where V_i and V_j refer to the volume content of gas before and after the reaction, respectively. Assuming that the gas temperature T is constant before and after detonation reaction, the equation of the state of perfect gas can be obtained as

Eq.(13), as follows:

$$P(V_j - V_i) = (n_j - n_i)RT \quad (13)$$

where R is the constant of the perfect gas, and n_i and n_j refer to the molar content of gas before and after the reaction, respectively. Q_p after detonation can be calculated by the enthalpy increase of the system, as expressed by Eq.(14):

$$Q_p = \sum n_j \Delta H_{fj}^0 - \sum n_i \Delta H_{fi}^0 \quad (14)$$

where ΔH_{fj}^0 and ΔH_{fi}^0 are standard molar enthalpies of detonation products and precursors, respectively. Assuming that the heat capacity at constant pressure C_v is only a function of temperature T , according to laws of thermodynamics, the detonation heat at constant pressure can be expressed by Eq.(15):

$$Q_v = \int_{T_i}^{T_j} C_v dT = t \bar{C}_v = (T_j - T_i) \sum n_j \bar{C}_{vj} \quad (15)$$

where T_j is the detonation temperature; T_i is the initial temperature; t is the temperature difference before and after detonation; C_{vj} is the average molecular thermal capacity at constant volume for detonation products. C_{vj} can also be expressed by Eq.(16), as follows:

$$\bar{C}_{vj} = a_j + b_j t \quad (16)$$

where a_j and b_j are the molecular constant volume heat capacity of detonation reaction product components. For C_v of all the detonation products, it can be summarized according to Eq.(17):

$$\bar{C}_v = A + Bt \quad (17)$$

where $A = \sum n_j a_j$ and $B = \sum n_j b_j$. Substituting Eq. (16) and Eq. (17) into Eq. (15), the detonation temperature can be obtained, as expressed by Eq.(18):

$$T_j - T_i = \frac{-A + \sqrt{A^2 + 4BQ_v}}{2B} \quad (18)$$

Table 1 shows the formation enthalpies of $TiCl_4$, TiO_2 , H_2O , and HCl at different temperatures. Table 2 shows the calculation results or relationship of average molecular

Table 1 Standard formation enthalpies of $TiCl_4$, TiO_2 , H_2O , and HCl (kJ/mol)^[22]

Substance	400 K	500 K
$TiCl_4$	-762.843	-762.501
Anatase- TiO_2	-936.286	-937.439
Rutile- TiO_2	-944.364	-943.603
H_2O	-223.951	-219.951
HCl	-92.581	-92.907

Table 2 Calculation results and relationship of average molecular thermal capacity at constant volume ($J \cdot mol^{-1} \cdot K^{-1}$)^[23]

Substance	C_v
Solid matter	24.9~25.4
Monatomic gas	20.77
Diatomic gas	20.0+0.001 88t
H_2O , H_2S	16.7+0.008 97t
CO_2 , SO_2	37.5+0.002 42t

thermal capacity at constant volume of different substances.

3 Results and Discussion

3.1 XRD analysis

Nineteen specimens were prepared under different conditions according to Table 3, and were named as S1~S19 in sequence.

The XRD patterns of prepared nano- TiO_2 products are shown in Fig. 2. The diffraction peaks at $2\theta=25.3^\circ$, 37.8° , 48.0° , 53.9° , and 62.7° correspond to the anatase- TiO_2 (according to JCPDS No. 99-0008), and those at $2\theta=27.4^\circ$, 36.0° , 41.2° , and 54.3° correspond to the rutile- TiO_2 (JCPDS No.99-0090). Therefore, it can be seen that all specimens have a mixed crystalline structure, except S9 and S13 which only possess rutile- TiO_2 phase. Fig. 2a shows XRD patterns of S1~S5 with preparation condition of $O_2:H_2:TiCl_4=1.0:1.0\sim 3.0:1.0$, presenting an upward trend for anatase- TiO_2 content but a downtrend for rutile- TiO_2 content with increasing the H_2 content. Fig. 2b shows XRD patterns of S6~S9 with the preparation condition of $O_2:H_2:TiCl_4=0.5\sim 2.0:2.0:1.0$, which have the similar trends of anatase- TiO_2 and rutile- TiO_2 contents with increasing the O_2 content, compared with those in Fig. 2a. Fig. 2c shows XRD patterns of S10~S13 with the preparation condition of $O_2:H_2:TiCl_4=1.0:2.0:0.5\sim 1.5$. The increasing $TiCl_4$ content leads to the decline in anatase- TiO_2 production but results in the augmentation in rutile- TiO_2 . Fig. 2d shows XRD patterns of S14~S16 with the preparation condition of $O_2:H_2:TiCl_4=1.0\sim 2.33:2.0\sim 4.66:1.0$. When the molar ratio of H_2 to O_2 is fixed and the $TiCl_4$ amount is unchanged, increasing initial pressure is conducive to the generation of rutile- TiO_2 . Fig. 2e shows XRD patterns of S17~S19 with the preparation condition of $O_2:H_2:TiCl_4=1.0:2.0:0.5\sim 1.5$. The change trends of anatase- TiO_2 and rutile- TiO_2 contents are similar to those in Fig. 2c, but the nano- TiO_2 crystalline structure is slightly different on account of the discrepancy in initial temperature.

The average crystal size of nano- TiO_2 powder can be calculated by the Scherrer equation: $D=K\lambda/\beta\cos\theta$, where D is the average crystal size of grains, K is a constant of 0.89, λ represents the X-ray wavelength, β represents the half-peak width of the corresponding diffraction peak, and θ represents the Bragg angle of diffraction peaks. The calculated results of average crystal size of nano- TiO_2 powder are shown in Table 3.

The crystal content of anatase- TiO_2 and rutile- TiO_2 from gaseous detonation can be calculated by Spurr and Myers formula^[24], as expressed by Eq.(19) and Eq.(20), respectively:

$$W_A = \frac{K_A I_A}{K_A I_A + I_R} \quad (19)$$

$$W_R = \frac{I_R}{K_A I_A + I_R} \quad (20)$$

where I_A represents the integrated intensity of the (101) peak of anatase- TiO_2 , I_R represents the height of (110) peak of rutile- TiO_2 , and K_A is a constant of 0.884. The calculated results are shown in Table 3.

Table 3 Preparation conditions, component proportions, and crystal sizes of S1~S19 specimens

Specimen	Initial temperature/K	Initial pressure/MPa	O ₂ :H ₂ :TiCl ₄	Content/wt%		Crystal size/nm	
				Anatase	Rutile	Anatase	Rutile
S1	423	0.1	1.0:2.0:1.0	45.8	54.2	26	37
S2	423	0.1	1.0:3.0:1.0	76.9	23.1	42	22
S3	423	0.1	1.0:2.5:1.0	67.3	33.7	38	20
S4	423	0.1	1.0:1.5:1.0	28.1	71.9	44	44
S5	423	0.1	1.0:1.0:1.0	11.4	88.6	55	49
S6	423	0.1	2.0:2.0:1.0	86.8	13.2	49	63
S7	423	0.1	1.5:2.0:1.0	77.9	22.1	53	59
S8	423	0.1	0.75:2.0:1.0	5.7	94.3	33	35
S9	423	0.1	0.5:2.0:1.0	-	-	-	-
S10	423	0.1	1.0:2.0:0.5	50.8	49.2	47	53
S11	423	0.1	1.0:2.0:0.75	47.7	52.3	50	49
S12	423	0.1	1.0:2.0:1.25	35.7	64.3	56	54
S13	423	0.1	1.0:2.0:1.5	0.1	99.9	-	46
S14	413	0.1	1.0:2.0:1.0	57.4	42.6	13	34
S15	413	0.15	1.66:3.22:1.0	56.3	43.7	20	40
S16	413	0.2	2.33:4.66:1.0	24.8	75.2	35	40
S17	413	0.1	1.0:2.0:1.5	15.7	84.3	34	45
S18	413	0.1	1.0:2.0:1.25	23.1	76.9	26	31
S19	413	0.1	1.0:2.0:0.5	76.5	23.5	10	21

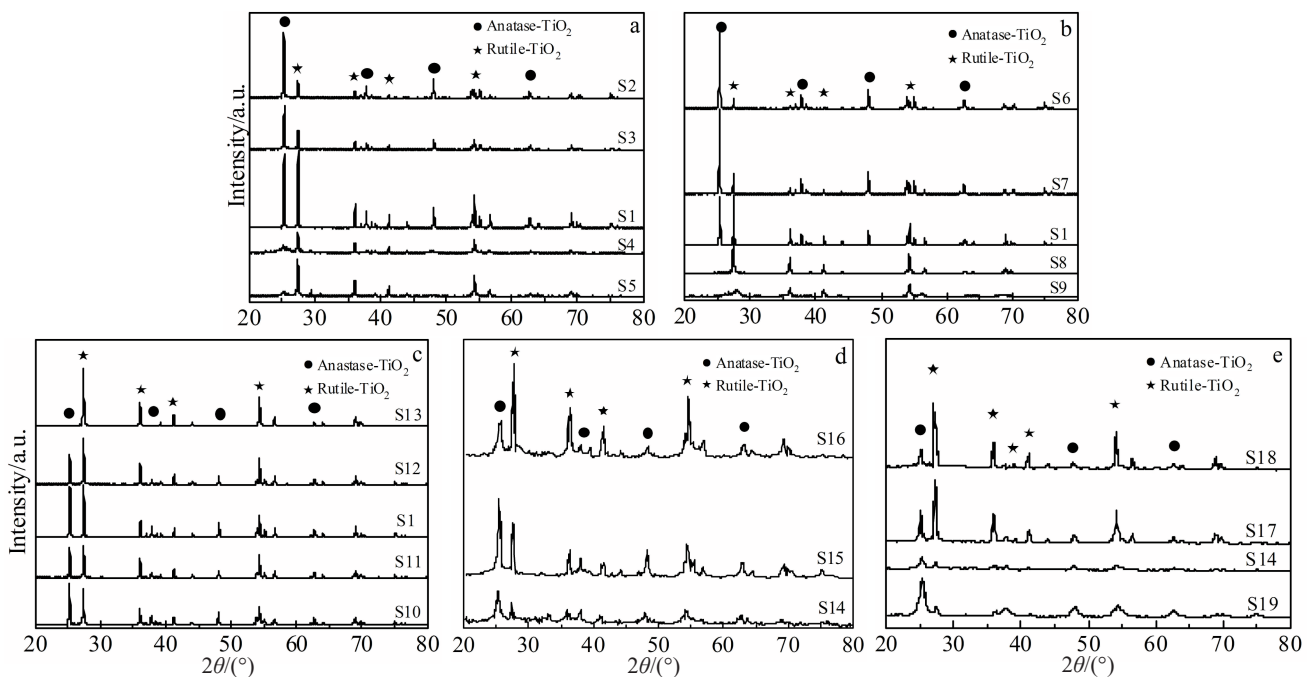


Fig.2 XRD patterns of S1~S5 (a), S6~S9 (b), S10~S13 (c), S14~S16 (d), and S17~S19 (e) specimens

3.2 TEM analysis

The microstructure of representative products S1, S6, and S13 was investigated by TEM, as shown in Fig.3. It can be seen that the nano-TiO₂ of S1 specimen has mixture phases of 45.8wt% anatase-TiO₂ and 54.2wt% rutile-TiO₂. The products consist of spherical or quasi-spherical nanoparticles with

particle size in a larger wide range of 20~150 nm. S6 specimen possesses good dispersity and relatively uniform crystal size of 40~60 nm. The main component of S6 specimen is anatase-TiO₂ (86.8wt%). It is also demonstrated that S13 specimen is pure rutile-TiO₂ and the average crystal size is 46 nm. The particle dispersity of S13 is relatively good,

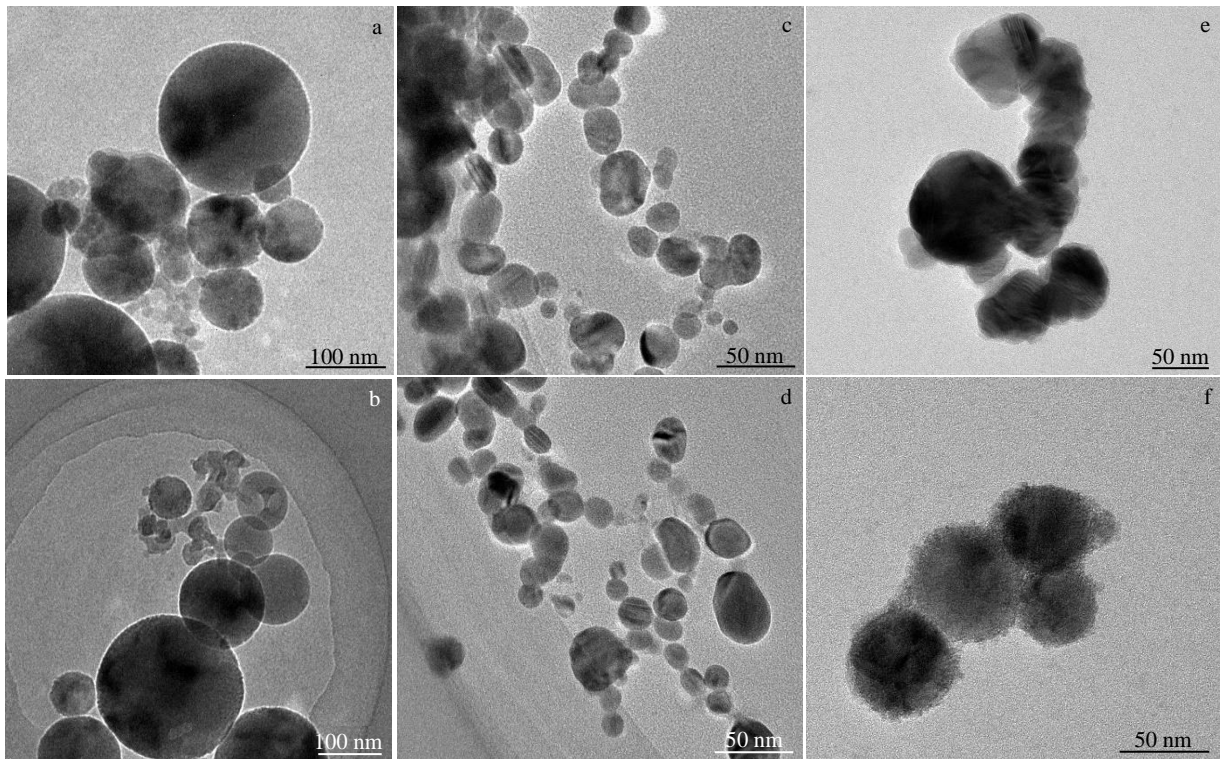


Fig.3 TEM images of S1 (a, b), S6 (c, d), and S13 (e, f) specimens

shows only a slight agglomeration.

3.3 Controllable synthesis of nano-TiO₂

Fig.4 shows the changing trend of anatase-TiO₂ content and rutile-TiO₂ content under different initial reaction conditions. Fig.4a shows that with solely increasing the H₂ content, the content of anatase-TiO₂ and rutile-TiO₂ is increased and decreased, respectively. Fig.4b shows that with solely increasing the O₂ content, the content of anatase-TiO₂ is also increased. Fig.4c and 4e show that with solely increasing the TiCl₄ content, the rutile-TiO₂ phase is increased while the anatase-TiO₂ phase is decreased, i.e., the transformation from anatase-TiO₂ to rutile-TiO₂ is enhanced. With solely increasing the initial pressure of H₂/O₂, the generation of rutile-TiO₂ is increased, as shown in Fig.4d. Compared with Fig.4a and 4b, it can be seen that when the content of H₂ or O₂ exceeds the content of TiCl₄, the amount of anatase-TiO₂ is effectively increased.

During the GLD process, the leading shock wave flows through unreacted gas mixtures may cause a series of violent chemical reactions. The detonation heat under the atmosphere of high temperature and high pressure is generated rapidly during GLD chemical reaction. The GLD parameters were calculated based on the C-J theory, as shown in Table 4. The calculated results show that the maximum detonation parameters of detonation temperature, detonation pressure, and detonation velocity are 4271 K, 7.33 MPa, and 2946 m/s, respectively. The detonation condition for obtaining pure rutile-TiO₂ is detonation temperature of 3583 K, detonation pressure of 3.36 MPa, and detonation velocity of 1823 m/s.

Under the atmosphere of instantaneous high temperature and high pressure, all the mixture precursors may decompose into ions and then form tiny TiO₂ which agglomerates to form nano-TiO₂ gradually^[25]. The results of thermodynamic calculation show that the phase stability of rutile-TiO₂ and anatase-TiO₂ decreases generally, which depends on the difference of surface energy. As long as the crystal size is small enough, the stability of anatase phase is stable^[26,27]. Zhao et al^[28] reported that the critical diameter of anatase phase is less than that of rutile phase during the detonation reaction process, the crystal nucleus of anatase phase is generated at first, and the grains gradually grow. Hanaor et al^[29] summarized that the transformation temperature is 400~1200 °C since the transformation temperature is determined by the raw materials and preparation methods. In addition, the conversion rate of anatase-TiO₂ to rutile-TiO₂ depends on time^[30]. The transformation kinetics is related to the temperature-time conditions during the GLD chemical reaction. However, it is very difficult to measure the reaction and transformation time of preparation of nano-TiO₂ during the GLD process. Thus, the reaction and transformation time can only be simply determined by detonation velocity. The effects of two main reactions and cations on the transformation of anatase-TiO₂ to rutile-TiO₂ in the process of GLD reaction were discussed in Ref. [31]. The status under two important conditions need to be discussed: (1) the half content of water vapor from reaction of H₂ and O₂ is less than the content of TiCl₄; (2) the half content of water vapor is more than or equal to the content of TiCl₄.

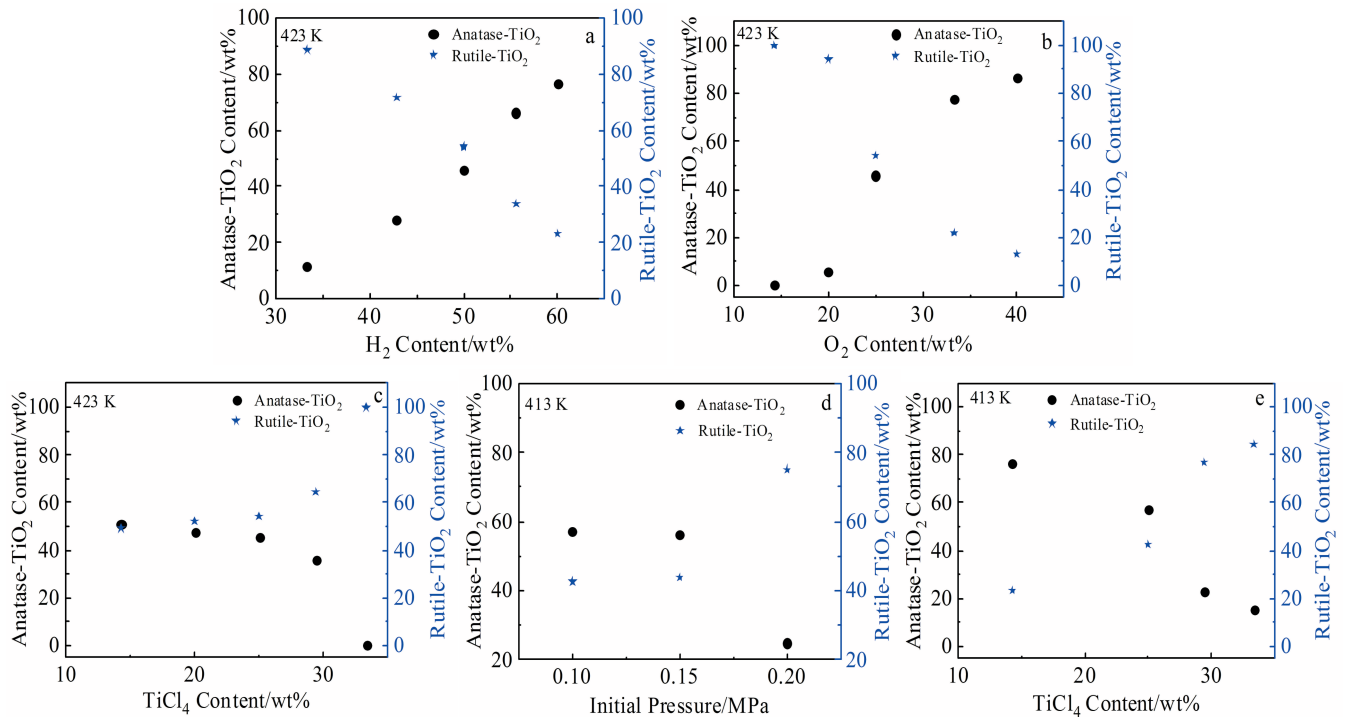


Fig.4 Influence of different initial reaction conditions on contents of anatase-TiO₂ and rutile-TiO₂; (a) H₂ content; (b) O₂ content; (c) TiCl₄ content at 423 K; (d) initial pressure; (e) TiCl₄ content at 413 K

Table 4 Calculated GLD parameters of S1~S19 specimens

Specimen	Detonation temperature/K	Detonation pressure/MPa	Detonation Velocity/m·s ⁻¹	Content/wt%	
				Anatase	Rutile
S1	4135	3.91	2212	45.8	54.2
S2	3553	3.15	2207	76.9	23.1
S3	3820	3.49	2210	66.3	33.7
S4	3878	3.72	2021	28.1	71.9
S5	3543	3.46	1808	11.4	88.6
S6	3553	3.15	2075	86.8	13.2
S7	3820	3.49	2140	77.9	22.1
S8	3572	3.25	1984	5.7	94.3
S9	2862	2.49	1706	-	-
S10	4252	4.15	2801	50.8	49.2
S11	4195	4.02	2445	47.7	52.3
S12	3846	3.62	1993	35.7	64.3
S13	3583	3.36	1823	-	99.9
S14	4144	3.42	2218	57.4	42.6
S15	4234	5.37	2639	56.3	43.7
S16	4271	7.33	2946	24.8	75.2
S17	3854	3.17	1999	15.7	84.3
S18	3591	2.95	1829	23.1	76.9
S19	4256	3.63	2806	76.5	23.5

Fig. 5a shows the variation of rutile-TiO₂ content and detonation velocity with calculated temperature under the former condition. The results show that the content of rutile-

TiO₂ by GLD method is related to detonation temperature and velocity. Initially, the content of rutile-TiO₂ is increased with increasing the detonation temperature. When the detonation

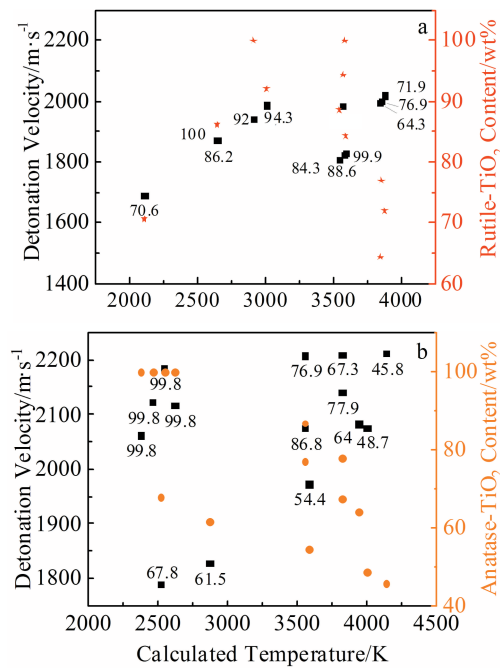


Fig.5 Variation of rutile-TiO₂ content and detonation velocity with calculated temperature under the former condition (a); variation of anatase-TiO₂ and detonation velocity with calculated temperature under the latter condition (b)

temperature is more than 3500 K, the content of rutile-TiO₂ products is reduced. It can be concluded that the rutile-TiO₂ of high purity is generated at detonation temperature of 3000~3500 K and the detonation velocity is 1800~2000 m/s under this condition. Fig.5b shows the variation of anatase-TiO₂ and detonation velocity with calculated temperature under the latter condition. The increasing temperature inhibits the formation of anatase-TiO₂, i.e., the formation of rutile-TiO₂ is promoted. On the other hand, when the alcohol solution is added into the mixture precursors (O₂:H₂:TiCl₄:C₂H₆O=1.0:2.0:1.0:0.3~0.6), the pure anatase-TiO₂ appears at temperature of 2400~2600 K and the detonation velocity is 2100~2200 m/s under this condition. The formation of pure anatase-TiO₂ is related to higher detonation velocity. During the GLD process, the transformation time of anatase-TiO₂ into rutile-TiO₂ is shortened, which is conducive to the formation of anatase-TiO₂, which is possibly related with the inhibitory effect of anion^[29].

4 Conclusions

1) Nano-TiO₂ of different crystal structures have spherical or quasi-spherical shapes with good dispersity, and the crystal size is 20~150 nm.

2) Under the conditions of stable gaseous-liquid detonation (GLD), when the content of H₂ or O₂ exceeds that of TiCl₄, the production of anatase-TiO₂ is increased. With the same ratio of H₂ to O₂, the increase of TiCl₄ content contributes to the formation of rutile-TiO₂. With increasing the initial pressure of H₂-O₂ and retaining the TiCl₄ content, the formation of rutile-

TiO₂ is increased.

3) The condition of detonation temperature of 2400~2600 K and detonation velocity of 2100~2200 m/s is conducive to the formation of anatase-TiO₂ when the half content of water vapor from reaction of H₂ and O₂ is more than or equal to the content of TiCl₄. When the half content of water vapor originating from reaction of H₂ and O₂ is less than the content of TiCl₄, the formation of rutile-TiO₂ is increased under the condition of detonation temperature of 3000~3500 K and detonation velocity of 1800~2000 m/s.

4) It is difficult to synthesize nano-TiO₂ with desired crystalline structure, i. e., the controllable accuracy of detonation reaction conditions and detonation parameters of GLD needs to be further verified.

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气液爆轰控制合成多晶纳米二氧化钛

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摘 要: 以氢气、氧气和四氯化钛为混合前驱体, 通过气液爆轰法合成了多晶纳米二氧化钛。研究了不同摩尔比例的前驱体和初始反应压力对纳米二氧化钛晶相结构的影响。采用X射线衍射及透射电子显微镜对产物的纳米结构、成分、颗粒大小和形态进行了表征。结果表明: 获得的二氧化钛存在纯净的锐钛矿相、纯净的金红石相和混合相, 其中混合相的球形或者类球形颗粒粒径为20~150 nm。分析了纳米二氧化钛在气液爆轰中的形成机制。基于C-J理论和化学反应数据, 计算了爆轰参数; 该参数验证了不同摩尔比例的前驱体和初始反应压力对控制合成多晶纳米二氧化钛的影响。

关键词: 纳米二氧化钛; 气液爆轰; 多晶纳米结构; 爆轰参数; C-J理论

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